

Nonlinear Dynamic Maximum Power Theorem,  
with Numerical Method

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ABSTRACT

This paper considers the problem of maximizing the energy or average power transfer from a nonlinear dynamic n-port source. The main theorem includes as special cases the standard linear result  $Y_{load} = Y_{source}^*$  and a recent finding for nonlinear resistive networks. An operator equation for the optimal output voltage  $\hat{v}(\cdot)$  is derived, and a numerical method for solving it is given.

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## I. Introduction

This paper addresses the problem of extracting the maximum energy or average power from a source with the topology shown in Fig. 1. As in<sup>1</sup> [1], the problem is formulated as finding the optimal output voltage  $\hat{v}(\cdot)$  for each current source waveform  $i_s(\cdot)$  rather than finding a load that maximizes the power.

The central result is the operator equation (6) for  $\hat{v}(\cdot)$ . Theorem 1 gives conditions that guarantee uniqueness and global optimality of the solution: the standard result for linear systems [1] and recent work on resistive nonlinear systems [2] follow as special cases. Equation (11) defines a practical algorithm for solving (6), and Theorem 2 gives conditions that guarantee convergence.

The solution  $\hat{v}(\cdot)$  can be of engineering value in two ways. First, the average power  $\bar{P}(\hat{v})$  tells us the optimal performance that is possible in principle. Second,  $\hat{v}(\cdot)$  itself is a concrete design goal. If the source admittance operator  $F$  is continuous, a load for which the output approximates  $\hat{v}(\cdot)$  (in the Hilbert space norm used in this work) will absorb an average power that approximates  $\bar{P}(\hat{v})$ .

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1. Reference [1] actually deals with the dual network, where the source appears in Thevenin form.

## II. Results

### 2.1) Notation and Definitions

Let  $L$  be any real inner product space and  $\hat{L}$  any linear subspace of  $L$ .  
An operator  $F: \hat{L} \rightarrow L$  is said to be

a) strictly increasing if

$$\langle F(y) - F(x), y-x \rangle > 0, \forall x \neq y \in \hat{L}, \quad (1)$$

b) uniformly increasing if for some  $\delta > 0$ ,

$$\langle F(y) - F(x), y-x \rangle \geq \delta \|y-x\|^2, \forall x, y \in \hat{L}, \quad (2)$$

c) Lipschitz continuous if for some  $K \geq 0$ ,

$$\|F(y) - F(x)\| \leq K \|y-x\|, \forall x, y \in \hat{L}. \quad (3)$$

Let  $L, L'$  be any real inner product spaces and  $L(L, L')$  denote the space of continuous linear maps from  $L$  to  $L'$ , with the operator norm [3, p.53].  
For  $A \in L(L, L')$ , let  $A^{\text{adj}}$  denote the adjoint of  $A$ .

Given an operator  $F: L \rightarrow L'$  and  $x, h \in L$ , suppose there exists an element denoted  $\delta F(x, h)$  of  $L'$  such that

$$\lim_{t \rightarrow 0^+} \left\| \frac{F(x+th) - F(x)}{t} - \delta F(x, h) \right\|_{L'} = 0.$$

Then  $\delta F(x, h)$  is called the Gâteaux variation of  $F$  at  $x$  for the increment  $h$  [4, p.251]. If  $\delta F(x, h)$  exists for all  $x, h \in L$ , and if for each  $x \in L$  the map  $h \rightarrow \delta F(x, h)$  is an element of  $L(L, L')$ , then  $F$  is said to be Gâteaux differentiable on  $L$ . In this case the map  $x \rightarrow \delta F(x, \cdot)$  is called the Gâteaux derivative of  $F$  and denoted  $DF: L \rightarrow L(L, L')$  [4, pp.255-256]. Similarly

$\delta F(x, \cdot)$  is denoted  $DF(x) \in L(L, L')$ , and  $\delta F(x, h)$  is denoted  $(DF(x))h \in L'$ . The value of using the Gateaux derivative rather than the more restrictive Fréchet derivative [4, Chap. 3] will become apparent in section 3.1.

The Hilbert space  $L_n^2$  is the set of all measurable functions  $\tilde{x}: \mathbb{R} \rightarrow \mathbb{R}^n$  such that the integral of  $\tilde{x}_j^2(\cdot)$  over  $\mathbb{R}$  is finite,  $j=1, \dots, n$ , equipped with the usual inner product  $\langle \cdot, \cdot \rangle$  and norm,  $\|\tilde{x}\| \triangleq \langle \tilde{x}, \tilde{x} \rangle^{1/2}$ .

For each  $T > 0$ ,  $L_{n,T}^2$  is the set of all periodic measurable functions  $\tilde{x}: \mathbb{R} \rightarrow \mathbb{R}^n$  with period  $T$  such that the integral over one period of  $\tilde{x}_j^2(\cdot)$  is finite,  $j=1, \dots, n$ . It is a Hilbert space with the "average power" inner product

$$\langle \tilde{x}, \tilde{y} \rangle_T \triangleq \frac{1}{T} \int_0^T \tilde{x}(t) \cdot \tilde{y}(t) dt, \quad (4)$$

where  $\tilde{x} \cdot \tilde{y}$  is the Euclidean inner product on  $\mathbb{R}^n$ . The norm on  $L_{n,T}^2$  is denoted  $\|\tilde{x}\|_T \triangleq \langle \tilde{x}, \tilde{x} \rangle_T^{1/2}$ .

## 2.2) Main Theorem

### Theorem 1 (Maximum Average Power in the Periodic Steady State)

Fix  $T > 0$  and let the  $n$ -port  $N_1$  in Fig. 1 be characterized by an admittance operator  $F: L_T \rightarrow L_T$ , where  $L_T$  is any linear subspace of  $L_{n,T}^2$ . Suppose  $F$  is Gateaux differentiable on  $L_T$  and that the associated operator  $H: L_T \rightarrow L_T$ , given by

$$H: \tilde{v} \mapsto F(\tilde{v}) + (DF(\tilde{v}))^{\text{adj}} \tilde{v}, \quad (5)$$

2. Thus, if  $\tilde{y}(\cdot)$  has period  $T$  and lies in  $L_{n,T}^2$ , the response  $\tilde{i}(\cdot)$  of  $N_1$  cannot have subharmonics.

is strictly increasing.

Then for each  $\tilde{i}_s \in H(L_T)$  there is a unique solution  $\hat{v}(\tilde{i}_s) \in L_T$  to

$$\tilde{i}_s = H(\tilde{v}), \quad (6)$$

and the average power<sup>3</sup> absorbed by the load,

$$\bar{P}(\tilde{v}) \triangleq \langle \tilde{i}_0, \tilde{v} \rangle_T = \langle \tilde{i}_s - F(\tilde{v}), \tilde{v} \rangle_T, \quad (7)$$

has a unique global maximum over  $L_T$ , which is attained at  $\tilde{v} = \hat{v}(\tilde{i}_s)$ .

#### Corollary (Maximum Total Energy for Transients)

Let  $L$  be a linear subspace of  $L_n^2$ , and substitute  $L$  for  $L_T$  in the assumptions of Theorem 1. Then the same conclusions<sup>4</sup> hold, but with  $\hat{v}(\tilde{i}_s) \in L$  maximizing the total energy  $E(\tilde{v}) \triangleq \langle \tilde{i}_s - F(\tilde{v}), \tilde{v} \rangle$  over  $L$ .

Note that in general  $F$  can be nonlinear and time-varying.

In applications one might wish to restrict attention to currents and voltages in  $L_{n,T}^2$  with additional properties such as continuity or boundedness. This is the reason for introducing  $L_T \subset L_{n,T}^2$  in the formulation of Theorem 1.

The essential idea behind the theorem is that a solution  $\hat{v}(\cdot)$  of (6) is a stationary point of  $\bar{P}: L_T \rightarrow \mathbb{R}$ , and the monotonicity assumption on  $H$  guarantees that  $\bar{P}$  is strictly concave. Details follow.

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3. A more explicit, but cumbersome, notation would be  $\bar{P}(\tilde{v}, \tilde{i}_s)$ . Using it, Theorem 1 states that  $\forall \tilde{v}, \tilde{i}_s \in L_T$ ,  $\bar{P}(\tilde{v}, \tilde{i}_s) < \bar{P}(\hat{v}(\tilde{i}_s), \tilde{i}_s)$  if  $\tilde{v} \neq \hat{v}(\tilde{i}_s)$ .

4. For the Corollary, the adjoint is of course taken with respect to the inner product on  $L_n^2$  rather than  $\langle \cdot, \cdot \rangle_T$ .

Proof of Theorem 1

Uniqueness of the solution to (6) follows from the fact that  $H$  is strictly increasing. By the chain rule for the composition of Fréchet- and Gâteaux-differentiable functions [4,p.253]  $\bar{P}$  is Gâteaux differentiable and for all  $\tilde{x}, \tilde{h} \in L_T$ ,

$$\begin{aligned} (\bar{D}\bar{P}(\tilde{x}))\tilde{h} &= \langle \tilde{i}_S - F(\tilde{x}), \tilde{h} \rangle_T - \langle (DF(\tilde{x}))\tilde{h}, \tilde{x} \rangle_T = \\ &= \langle \tilde{i}_S - F(\tilde{x}) - (DF(\tilde{x}))^{\text{adj}} \tilde{x}, \tilde{h} \rangle_T = \\ &= \langle \tilde{i}_S - H(\tilde{x}), \tilde{h} \rangle_T. \end{aligned} \quad (8)$$

Thus if  $\tilde{i}_S \in H(L_T)$ ,

- a)  $\bar{D}\bar{P}(\hat{v}(\tilde{i}_S)) = 0 \in L(L_T, L_T)$ ,
- b) given any  $\tilde{x}, \tilde{y} \in L_T$ , the map  $\lambda \rightarrow \bar{P}[\tilde{x} + \lambda(\tilde{y} - \tilde{x})]$  is differentiable at each  $\lambda \in \mathbb{R}$ , and
- c)  $\frac{d}{d\lambda} \bar{P}[\tilde{x} + \lambda(\tilde{y} - \tilde{x})] = \langle \tilde{i}_S - H[\tilde{x} + \lambda(\tilde{y} - \tilde{x})], (\tilde{y} - \tilde{x}) \rangle_T$ .

To show that  $\hat{v}(\tilde{i}_S)$  globally optimizes  $\bar{P}$ , fix  $\tilde{i}_S \in H(L_T)$ , let  $\hat{v} = \hat{v}(\tilde{i}_S)$ , and choose any  $\tilde{v} \in L_T$ ,  $\tilde{v} \neq \hat{v}$ . Then

$$\begin{aligned} \bar{P}(\tilde{v}) - \bar{P}(\hat{v}) &= \\ \bar{P}[\hat{v} + \lambda(\tilde{v} - \hat{v})] \Big|_{\lambda=1} - \bar{P}[\hat{v} + \lambda(\tilde{v} - \hat{v})] \Big|_{\lambda=0} &= \\ \int_0^1 \left\{ \frac{d}{d\lambda} \bar{P}[\hat{v} + \lambda(\tilde{v} - \hat{v})] \right\} d\lambda. \end{aligned} \quad (9)$$

Using c), the integrand above is

$$\langle \tilde{i}_s - H[\tilde{v} + \lambda(\tilde{v} - \hat{v})], \tilde{v} - \hat{v} \rangle_T =$$

(since  $\tilde{i}_s = H(\hat{v})$ )

$$-\frac{1}{\lambda} \langle H[\tilde{v} + \lambda(\tilde{v} - \hat{v})] - H(\hat{v}), [\tilde{v} + \lambda(\tilde{v} - \hat{v})] - [\hat{v}] \rangle_T, \forall \lambda > 0,$$

and the integrand vanishes at  $\lambda=0$ . The inner product above is strictly positive for  $\lambda \neq 0$  since  $H$  is strictly increasing by assumption. Thus the integrand in (9) is negative for  $\lambda > 0$  and zero for  $\lambda=0$ , so  $\bar{P}(\tilde{v}) < \bar{P}(\hat{v})$  as claimed. ■

The proof of the Corollary is essentially identical and will be omitted.

### 2.3) Relation to "Impedance Matching" Ideas

The emphasis in this paper is on finding the optimal output voltage  $\hat{v}(\cdot)$ , not the optimal load. But the relation to impedance matching ideas deserves comment.

If the load in Fig. 1 is taken to be the (generally noncausal) admittance  $G_{\text{opt}}: L_T \rightarrow L_T$ , defined by

$$G_{\text{opt}}: \tilde{v} \mapsto (DF(\tilde{v}))^{\text{adj}} \tilde{v}, \quad (10)$$

then the network is uniquely solvable given any  $\tilde{i}_s \in H(L_T)$ , and the output voltage  $\tilde{v}(\cdot)$ , which necessarily equals  $\hat{v}(\tilde{i}_s)$ , globally optimizes  $\bar{P}$ . This generally noncausal load is "matched" to the source for all inputs  $\tilde{i}_s \in H(L_T)$ , and this result holds generally for a nonlinear, time-varying, even noncausal source admittance  $F$ . The reader can easily verify that in the LTI case (10) reduces to the standard linear theorem  $Y_{\text{load}}(j\omega) = Y_{\text{source}}^*(j\omega)$ . More detail for the linear 1-port case is given in Section 3.1.



Of course in practice one has a causal load, usually predetermined, and wishes to couple it to the source through a lossless matching network designed to maximize the absorbed power over a range of inputs. In the linear case this important problem is called "broadband matching" [5-8]. We note that in both the linear and nonlinear cases the problem can be viewed as compensating or coupling to a predetermined load using lossless elements in such a way that the response approximates that of the noncausal exact match  $\underline{G}_{opt}$  over the input range of interest.

For a particular drive  $\underline{i}_s$ , the situation is somewhat different. The optimal voltage  $\hat{\underline{v}}(\cdot)$  is unique, but the optimal load is not: the only requirement on  $\underline{G}$  is that  $\underline{G}(\hat{\underline{v}}) = \underline{G}_{opt}(\hat{\underline{v}})$ . In the linear case where  $\underline{F}$  and  $\underline{G}$  are respectively represented by admittance matrices  $\underline{Y}_S(j\omega)$  and  $\underline{Y}_L(j\omega)$ , there are in general infinitely many optimal, positive semidefinite choices of  $\underline{Y}_L$  at a given  $\omega$  for which the network is uniquely solvable [9]. The problem of finding solutions in particular classes, such as the class of resistive loads, is studied in [10].

## 2.4) Numerical Algorithm

Equation (8) shows that  $\underline{i}_s - \underline{H}(\underline{v})$  is the gradient [3,p.72], [4,p.196] of  $\bar{P}$  at  $\underline{v}$ ,  $\forall \underline{i}_s, \underline{v} \in L_T$ . This suggests that we attempt to maximize  $\bar{P}$  by a simple "hill-climbing" algorithm of the form

$$\underline{x}_{j+1} = \lambda(\underline{i}_s - \underline{H}(\underline{x}_j)) + \underline{x}_j \triangleq \underline{M}(\underline{x}_j) \quad (11)$$

for some  $\lambda > 0$ . Note that under the assumptions of Theorem 1, if  $\underline{x}_j \rightarrow \underline{x} \in L_T$  and  $\underline{H}$  is continuous, then  $\underline{i}_s = \underline{H}(\underline{x})$  and  $\underline{x}$  globally maximizes  $\bar{P}$ . By tightening the assumptions a little further, we can guarantee convergence for all

sufficiently small positive  $\lambda$ .

### Theorem 2

Strengthen the assumptions of Theorem 1 by supposing further that  $L_T$  is closed and  $H$  is uniformly increasing and Lipschitz continuous on  $L_T$ . (See (2), (3).) Then for any  $i_s \in L_T$ , any initial guess  $x_0 \in L_T$ , and any  $\lambda \in (0, 2\delta/K^2)$ , the sequence generated by (11) converges to  $\hat{v}(i_s)$ .

### Remark

Note that Theorem 2 also guarantees existence of a solution to (6) for all  $i_s \in L_T$ , i.e.,  $H(L_T) = L_T$ .

### Proof

Since  $L_T \subset L_{n,T}^2$  is closed and  $L_{n,T}^2$  is complete,  $L_T$  is complete [11]. It remains to show that  $M$  is contractive, i.e., that for some  $C < 1$ ,

$$\|M(y) - M(x)\|_T \leq C \|y - x\|_T, \quad \forall x, y \in L_T, \quad (12)$$

to guarantee  $\|x_n - \hat{v}(i_s)\|_T \rightarrow 0$  by the contraction mapping theorem [3,p.102], [12,p.28]. But

$$\begin{aligned} \|M(y) - M(x)\|_T^2 &= \\ \langle y - x - \lambda(H(y) - H(x)), y - x - \lambda(H(y) - H(x)) \rangle_T &= \\ \|y - x\|_T^2 - 2\lambda \langle H(y) - H(x), y - x \rangle_T + \lambda^2 \|H(y) - H(x)\|_T^2 &\leq \end{aligned}$$

$$(1 - 2\lambda\delta + \lambda^2 K^2) \|y-x\|_T^2 \triangleq C^2(\lambda) \|y-x\|_T^2,$$

and  $C^2(\lambda) < 1, \forall \lambda \in (0, 2\delta/K^2).$

### III. Examples

#### 3.1) Linear Operators and Memoryless Operators

Consider the time-invariant scalar case for simplicity, and let  $L_T^2$  stand for  $L_{1,T}^2$ .

If  $F_\ell$  is the convolution operator:  $v \mapsto a * v$  where  $a: \mathbb{R} \rightarrow \mathbb{R}$  is absolutely integrable, then for each  $T > 0$ ,  $F_\ell$  is a continuous linear operator:  $L_T^2 \rightarrow L_T^2$  and therefore Gateaux (in fact, Fréchet) differentiable. Since  $F_\ell$  is linear  $DF_\ell(x) \equiv F_\ell$ , and the reader can easily verify that  $(DF_\ell(x))^{\text{adj}} = F_\ell^{\text{adj}}: v(\cdot) \mapsto a(-\cdot) * v(\cdot)$ , i.e., the adjoint operation turns the impulse response around in time. Furthermore,  $H_\ell: v(\cdot) \mapsto [a(\cdot) + a(-\cdot)] * v(\cdot)$  is strictly increasing on  $L_T^2$  for each  $T > 0$  iff  $\text{Re} \{ \hat{a}(j\omega) \} > 0$  for all  $\omega$ , where  $\hat{a}$  is the Fourier transform of  $a$ . This follows from a slight modification of [12:pp.25, 174,235]. Similar results hold if  $a(\cdot)$  contains impulse functions as well [12:pp.246-247]. Thus  $G_{\text{opt}}: v(\cdot) \mapsto a(-\cdot) * v(\cdot)$ , and  $G_{\text{opt}}$  is represented in the frequency domain by the complex admittance  $\hat{a}^*(j\omega)$ . Therefore Theorem 1 and equation (10) reduce to the standard result  $Y_{\text{load}}(j\omega) = Y_{\text{source}}^*(j\omega)$  if  $F_\ell$  is linear and time-invariant.

Suppose  $F_m$  is memoryless but possibly nonlinear, i.e.,  $N_1$  is a resistor with the constitutive relation  $i=b(v)$ . Assume that  $b: \mathbb{R} \rightarrow \mathbb{R}$  is differentiable and its derivative  $b'(\cdot)$  is bounded. Then  $b$  is Lipschitz continuous on  $\mathbb{R}$  and hence for each  $T > 0$  the operator  $F_m: v(t) \mapsto b(v(t))$  maps  $L_T^2$  into  $L_T^2$ . Using Prop. 13 of [13:p.85] and the Lebesgue Convergence Theorem [13:p.88],

one can show that  $F_m$  is Gateaux differentiable on  $L_T^2$  and that for all  $x, y \in L_T^2$ ,  $(DF_m(x))y = y(\cdot)b'(x(\cdot)) \in L_T^2$ . Furthermore if  $h: v \mapsto b(v) + vb'(v)$  is a strictly increasing function on  $\mathbb{R}$ , then  $H_m: v(t) \mapsto b(v(t)) + v(t)b'(v(t))$  is a strictly increasing operator:  $L_T^2 \rightarrow L_T^2$ . Thus Theorem 1 reduces in this case to the result in [2].

The reader can easily check that  $DF_m: L_T^2 \rightarrow L(L_T^2, L_T^2)$  is not continuous unless  $b'(\cdot)$  is constant. Thus if  $N_1$  is a resistor with any nonlinearity (other than the trivial  $i = gv + \tilde{i}$ ),  $F_m$  is not Fréchet differentiable [4, Chap. 3] on  $L_T^2$ . This is the reason Theorem 1 was formulated in terms of the weaker Gateaux derivative.

### 3.2) Positive Linear Combinations of Operators

The (noncausal) matched load (10) for the source admittance  $F$  is related to  $F$  by a mapping  $\ell$ ,  $\ell(F) = G_{opt}^{adj}: v \mapsto (DF(v)) v$ . Note that  $\ell$  is linear; i.e.  $\ell(aF_1 + bF_2) = a\ell(F_1) + b\ell(F_2)$ . Given  $F_1$  and  $F_2: L_T \rightarrow L_T$ , consider  $F \triangleq aF_1 + bF_2$ . The reader can easily verify that if  $F_1, F_2$  satisfy the conditions of Theorem 1 (resp. Theorem 2), then  $F$  also satisfies Theorem 1 (resp. Theorem 2), provided  $a \geq 0, b \geq 0, a + b > 0$ .

For example, consider the source shown in Fig. 2, where  $N_1$  consists of the parallel connection of an LTI 1-port and a nonlinear resistor. If  $Y$  and  $g$  satisfy the conditions in section 3.1), then the (noncausal) matched load has the form shown in Fig. 2.

### 3.3) Circuit Example

Suppose the source takes the specific form in Fig. 3, with the resistor curves shown in Fig. 4. The convolution kernel  $a(t) = e^{-t}$ ,  $t \geq 0$ , for the

series connection of inductor and resistor satisfies the assumptions of section 3.1. The resistor curves  $g_k$  are differentiable everywhere and

$$h_k(v) \triangleq g_k(v) + v g_k'(v) = (k+1)v|v|^{k-1}, \quad k = 1, 2, 3, \quad (13)$$

with  $h_1(0) = 0$ . All the assumptions of section 3.1 are satisfied except that the derivatives  $g_2'(\cdot)$  and  $g_3'(\cdot)$  are unbounded. (Since they are bounded on every bounded subset of  $\mathbb{R}$ , a more detailed argument, omitted here, shows that the solutions obtained below maximize  $\bar{P}$  over  $L_T^\infty \cap L_T^2$ , which is certainly sufficient in practice.)

To find the optimal output  $\hat{v}$  in the three cases, we carried out the iterative procedure (11), which becomes in this instance

$$x_{j+1}(t) = \lambda \left[ 6 \sin(t) - (k+1)x_j(t)|x_j(t)|^{k-1} - \int_{-\infty}^{\infty} e^{-|t-\tau|} x_j(\tau) d\tau \right] + x_j(t), \quad k = 1, 2, 3. \quad (14)$$

Miss Pearl Yew of MIT has written a program in PASCAL to do the numerical solution. It was run on the DEC 20 in MIT's Research Laboratory of Electronics with an initial guess of  $x_0(\cdot) \equiv 0$ , and found to converge fairly rapidly for small positive values of  $\lambda$ . The results are shown in Fig. 5.

Since  $g_1$  represents a linear resistor, it follows from the traditional linear theorem that  $\hat{v}(t) = 2\sin(t)$  for  $k=1$ , in agreement with the numerical solution. Note that the instantaneous current drained by the nonlinear source resistor increases in magnitude with  $k$  for  $|v| > 1$  but decreases for  $|v| < 1$ . Thus it is intuitively reasonable that the optimal output spends a progressively greater percentage of time in the region  $|v| < 1$  as  $k$  increases.

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Figure Captions

- Fig. 1 The solution of the operator equation (6), given a particular  $i_s(\cdot)$ , is the optimal output voltage  $\hat{v}(\cdot)$ . It can be achieved with a variety of loads.
- Fig. 2 The optimal load admittance is obtained by a linear operator  $\mathcal{L}$  on the source admittance. Thus the optimal load for a parallel connection of source admittances is the parallel connection of the optimal loads for each source separately.
- Fig. 3 Theorems 1 and 2 let us numerically determine the optimal output voltage  $\hat{v}(\cdot)$  for this circuit when the resistor curves are as shown in Fig. 4.
- Fig. 4 The three resistor curves for the circuit in Fig. 3 are  $g_k(v) \triangleq v|v|^{k-1}$ ,  $k=1,2,3$ , with  $g_1(0) \triangleq 0$ .
- Fig. 5 One period of the optimal output voltages for the circuit in Fig. 3.

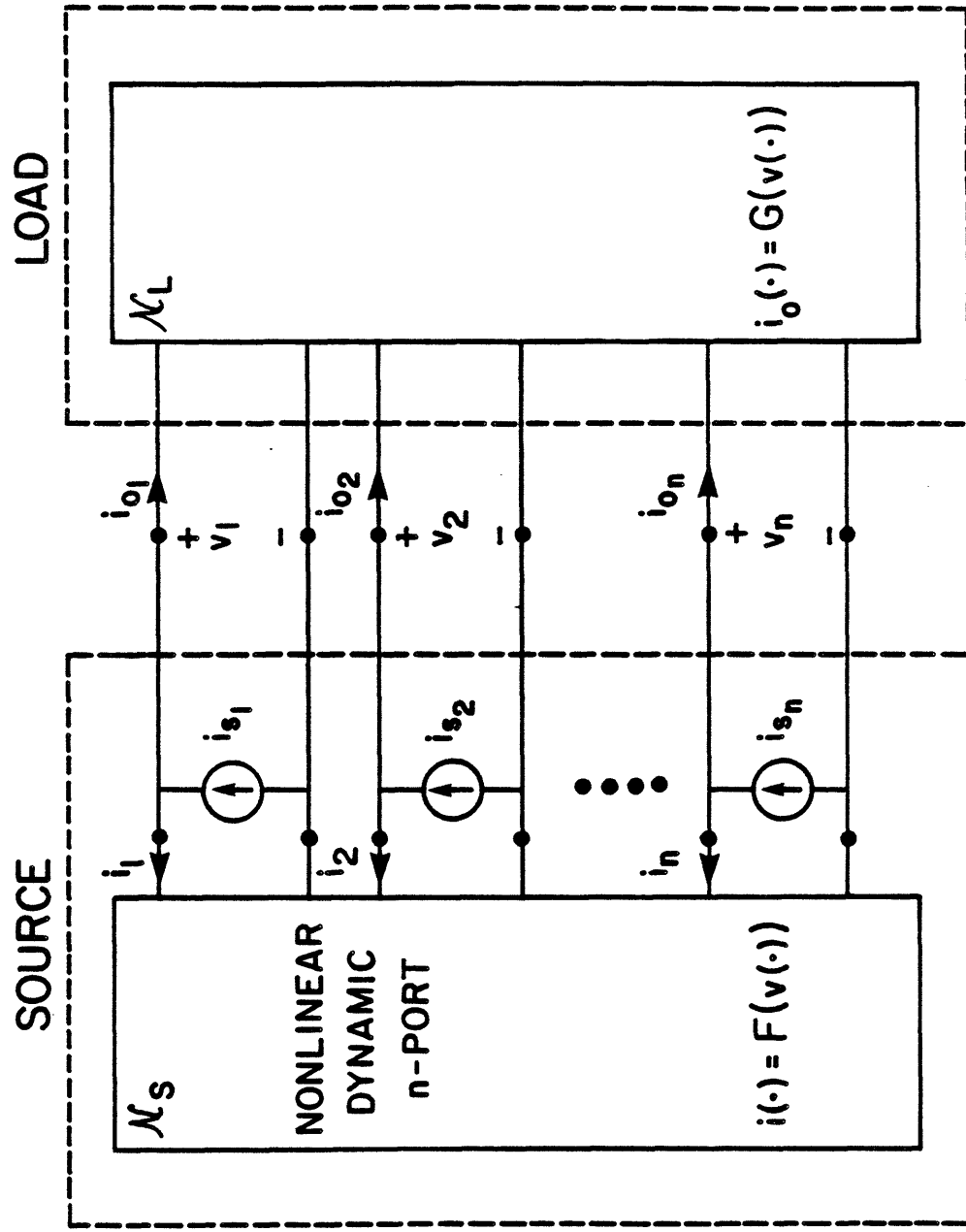


Figure 1



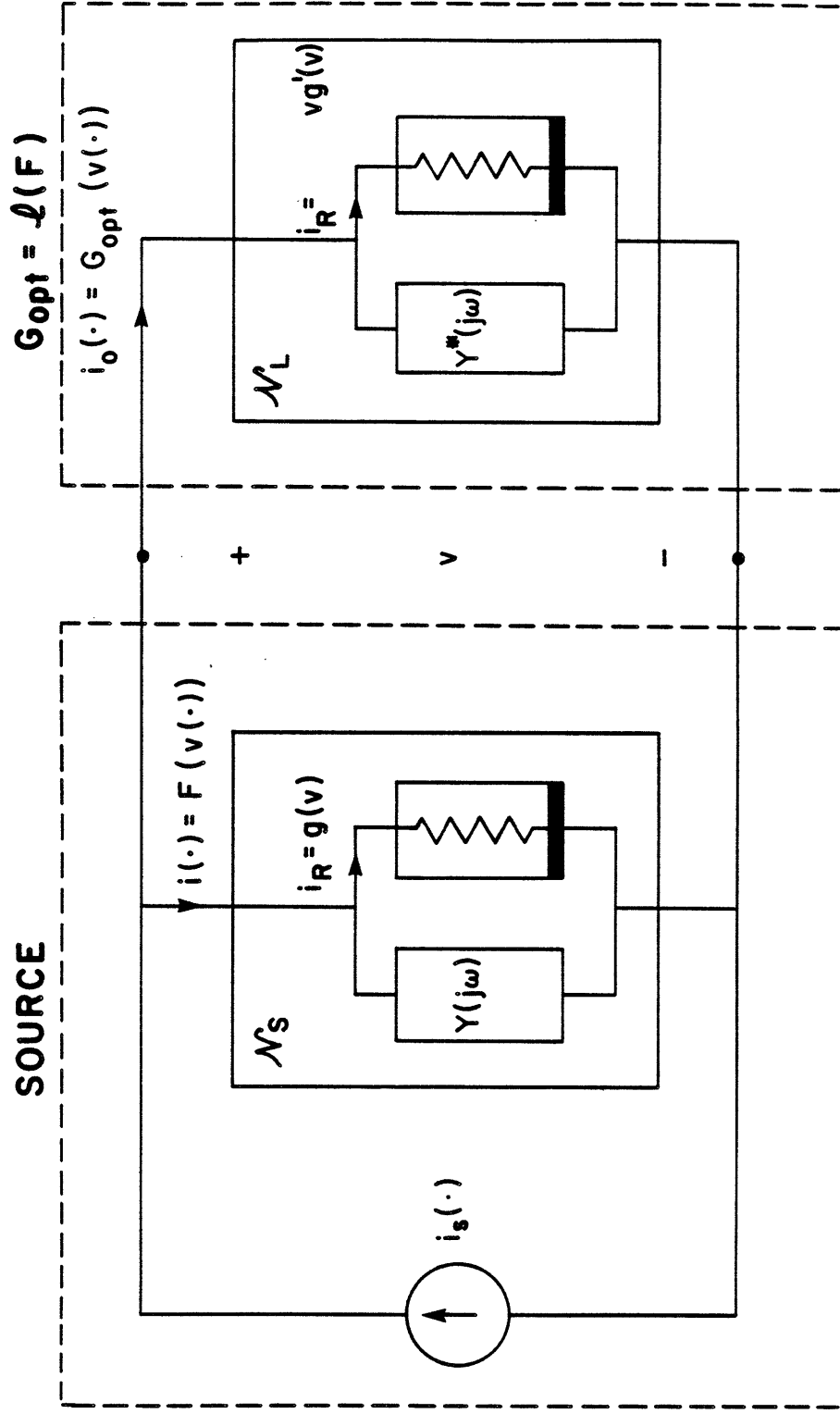


Figure 2

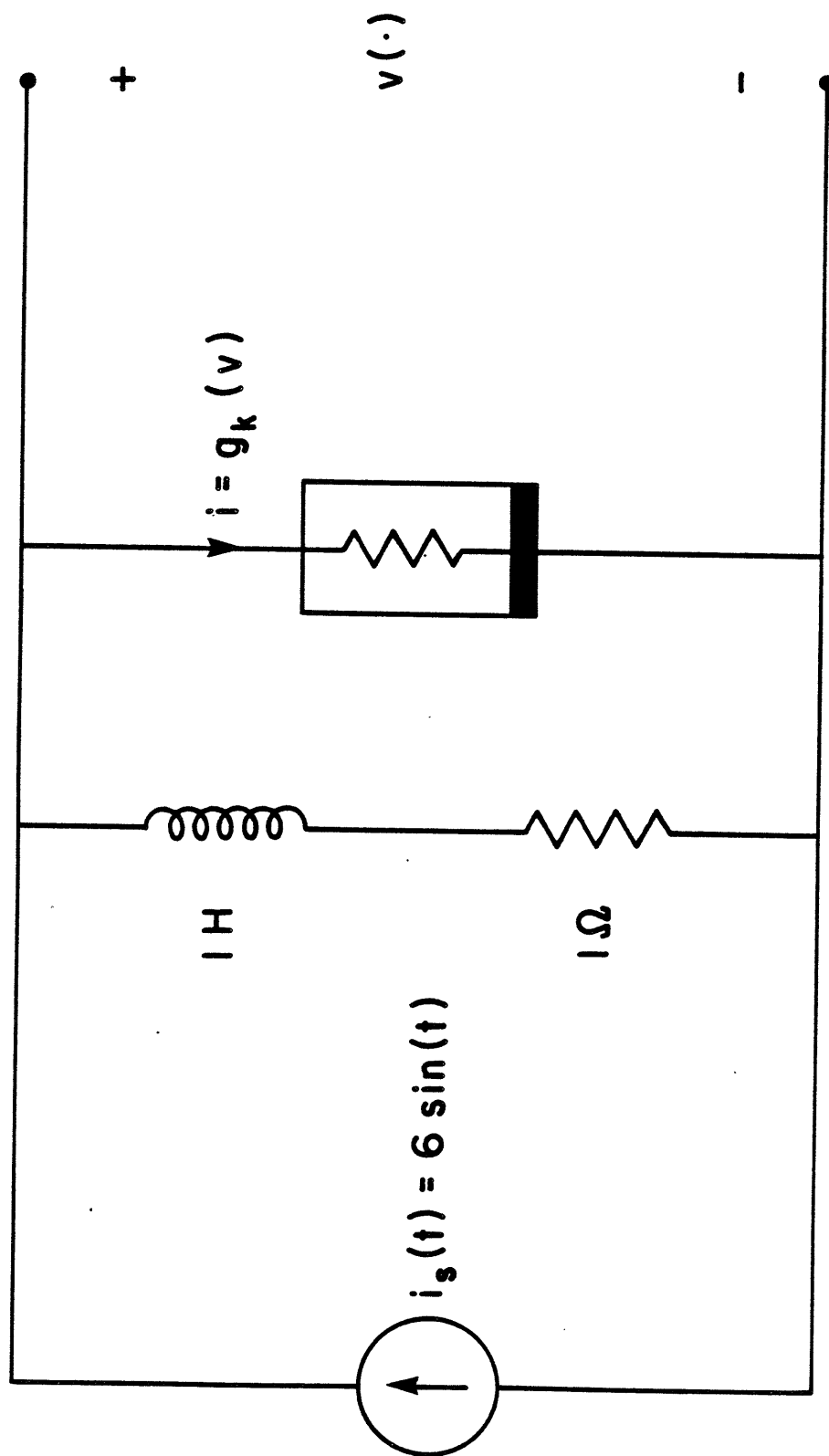


Figure 3

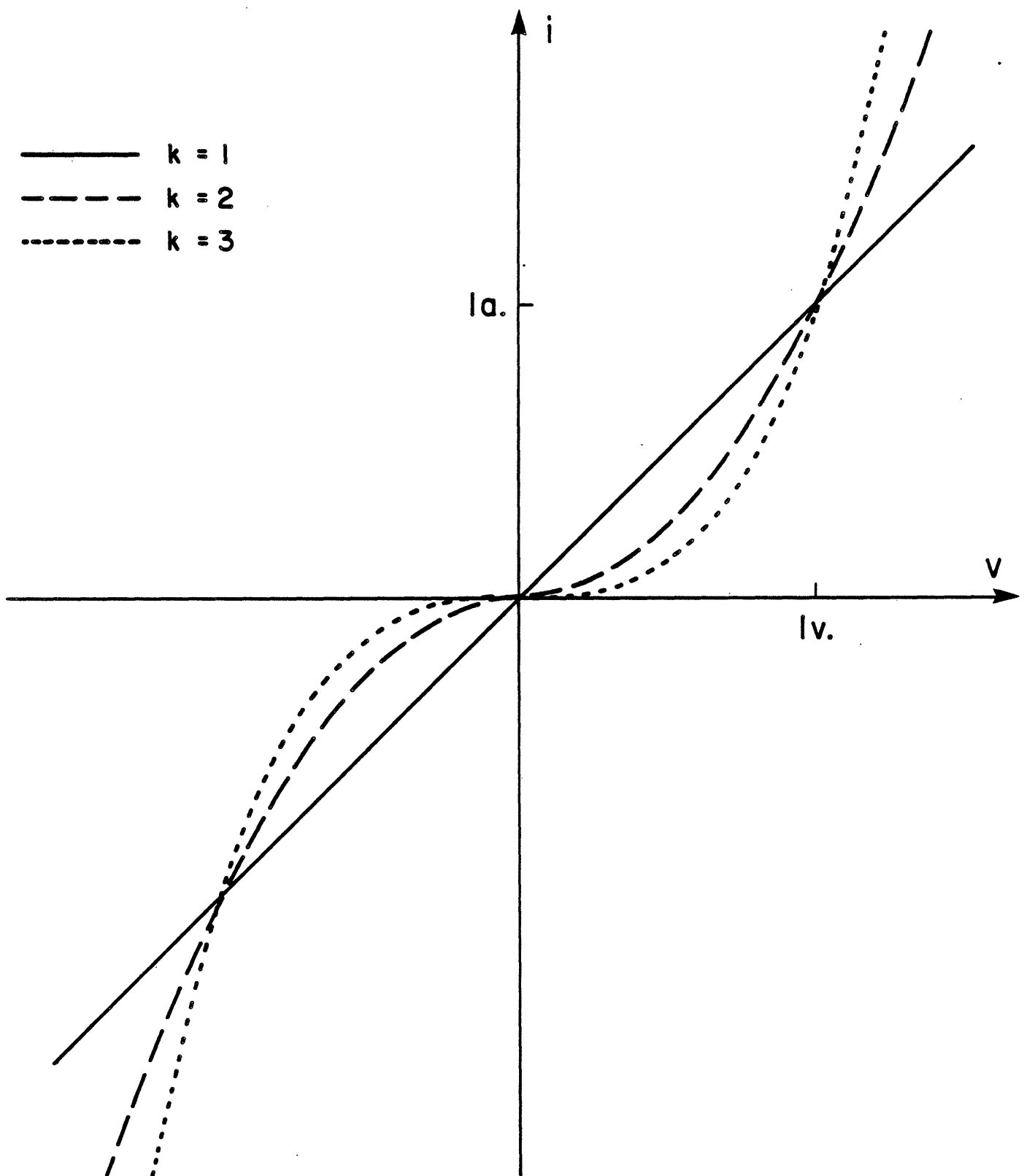


Figure 4

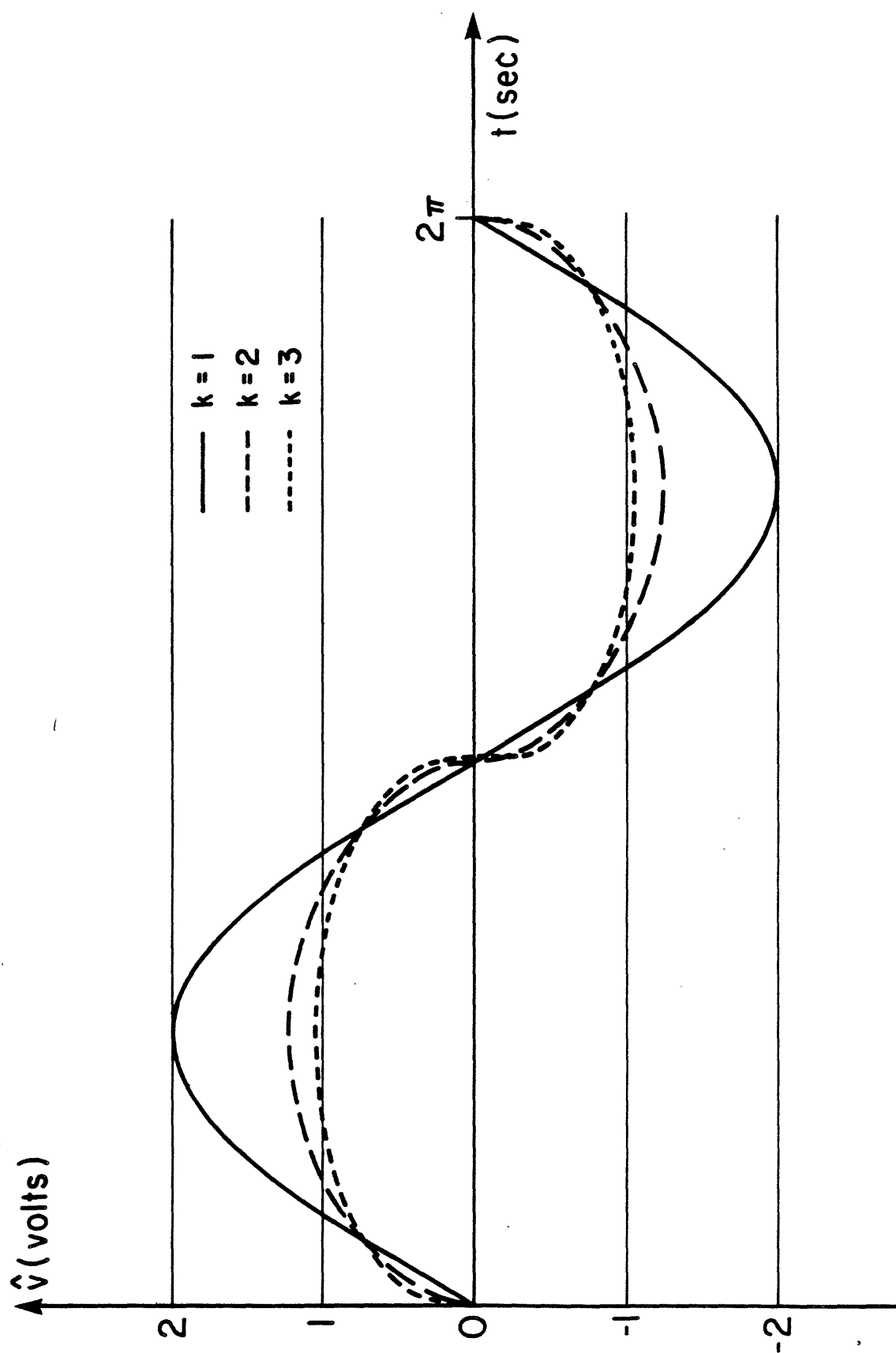


Figure 5